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Kinematics

An Overview for Wheeled Robots

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Structure

- ▶ Kinematics introduction
- ▶ Differential drive kinematics
- ▶ Motion constraints



Kinematics Introduction



What is Kinematics?

- ▶ For any mobile structure, it is important to **know how the structure can move around in space**
- ▶ The simplest way of studying motion is to **consider mathematical motion models that take into account the geometry of the structure and analyse motion under changing velocity** — this is the objective of kinematic models
- ▶ This is in contrast to **dynamics modelling, where forces / torques are considered as well**
- ▶ The primary use of kinematics models is that of **predicting the evolution of a robot's pose based on applied platform or individual wheel velocities**

Kinematics “relates to pure motion, i.e. to motion considered abstractly, without reference to force or mass” (Oxford Dictionary)

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Forward kinematics

A forward kinematics model **predicts the motion of a mobile base as a result of the motion of the individual wheels**

NB: In the context of robot manipulation, forward kinematics allows calculating the pose of the end effector based on the velocities of the manipulator's joints

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Inverse kinematics

An inverse kinematics model **identifies the required motions of the individual wheels so that the mobile base can move in a particular way**

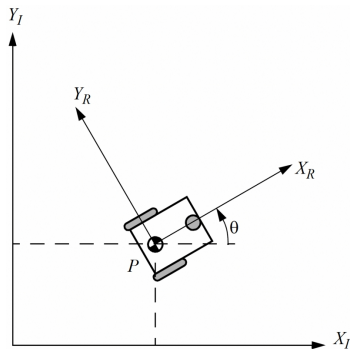
NB: In the manipulation context, inverse kinematics is concerned with calculating joint velocities that would result in a desired motion of the end effector

Robot Motion in Global and Local Coordinate Frames



- ▶ In a 2D plane, the pose ${}^I\mathbf{p}$ of a robot with respect to a global reference frame I is summarised by **the robot's position and planar orientation**: ${}^I\mathbf{p} = (x, y, \theta)^T$
- ▶ A robot's velocity vector ${}^I\dot{\mathbf{p}}$ with respect to I can be mapped to a velocity vector with respect to a robot's local frame R using a rotation matrix ${}^R_I R(\theta)$:

$${}^R\dot{\mathbf{p}} = {}^R_I R(\theta) {}^I\dot{\mathbf{p}} = \begin{pmatrix} \cos(\theta) & \sin(\theta) & 0 \\ -\sin(\theta) & \cos(\theta) & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \end{pmatrix}$$



A robot with a local reference frame R at a reference point P , rotated about an angle θ with respect to a global reference frame I

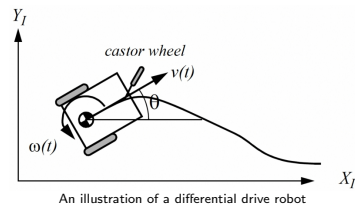
Differential Drive Kinematics



Differential Drive Robot



- ▶ A differential drive robot is a structure with **two active wheels**
 - ▶ Additional passive wheels may be included for stability
- ▶ The controllable wheels of a differential drive robot are **standard wheels** with an equal radius r
- ▶ We further consider that the wheels are **at a distance l from a point P that is centered between the wheels' axes**
- ▶ We consider **the velocities $\dot{\varphi}_1$ and $\dot{\varphi}_2$ of the wheels to be controllable**



Linear Motion



- ▶ First of all, note that, for a given angular velocity $\dot{\varphi}$, **a wheel with a radius r will have a forward linear velocity of $v_x = r\dot{\varphi}$**



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- ▶ A differential drive robot cannot move sideways, so $v_y = 0$

Angular Motion



- ▶ Robots rotate with a speed ω around a point called **instantaneous center of rotation (ICR)**
 - ▶ For a differential drive robot, if one of the wheels is static, the other wheel rotates in a **circular arc around the static wheel** (an arc of radius $2l$)



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- ▶ The distance D of P to the ICR can also be found as

$$D = l \frac{r\dot{\varphi}_1 + r\dot{\varphi}_2}{r\dot{\varphi}_1 - r\dot{\varphi}_2}$$

Forward Kinematics Model



- ▶ The complete forward kinematics model of a differential drive platform is given as

$${}^R\dot{\mathbf{p}} = \begin{pmatrix} \frac{r\dot{\varphi}_1}{2} + \frac{r\dot{\varphi}_2}{2} \\ 0 \\ \frac{r\dot{\varphi}_1}{2l} - \frac{r\dot{\varphi}_2}{2l} \end{pmatrix}$$



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- ▶ With respect to the global reference frame I , the model is given as

$${}^I\dot{\mathbf{p}} = R(\theta)^T {}^R\dot{\mathbf{p}} = R(\theta)^T \begin{pmatrix} \frac{r\dot{\varphi}_1}{2} + \frac{r\dot{\varphi}_2}{2} \\ 0 \\ \frac{r\dot{\varphi}_1}{2l} - \frac{r\dot{\varphi}_2}{2l} \end{pmatrix}$$

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- ▶ There are two concrete **constraints on the instantaneous wheel motion** that can provide useful information about a robot's motion:

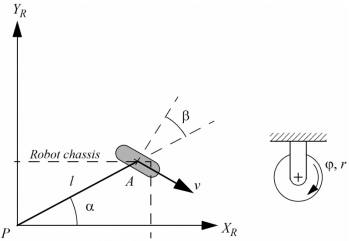
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- ▶ There are two concrete **constraints on the instantaneous wheel motion** that can provide useful information about a robot's motion:
 - ▶ **Rolling constraint**, which specifies a wheel's rolling motion (motion parallel to the wheel's plane) with respect to P
 - ▶ **Sliding constraint**, which specifies a wheel's sideways sliding motion (motion orthogonal to the wheel's plane) with respect to P

Standard Wheel Constraints

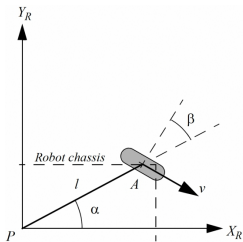


Standard Wheel Constraints

- ▶ For a fixed standard wheel, the motion parallel to the wheel's plane is captured by the wheel's rolling, so

Rolling constraint for a fixed standard wheel

$$\begin{pmatrix} \sin(\alpha + \beta) & -\cos(\alpha + \beta) & -l \cos(\beta) \end{pmatrix} {}^R_I R(\theta)^I \dot{\mathbf{p}} = r \dot{\phi}$$



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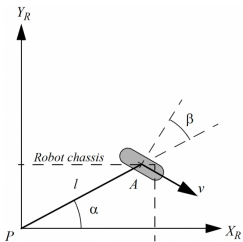
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- ▶ A standard wheel cannot slide sideways; thus, the velocity orthogonal to the wheel's plane needs to be equal to 0:

Sliding constraint for a fixed standard wheel

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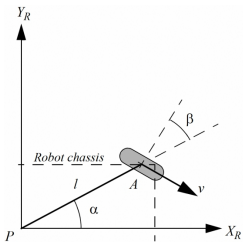
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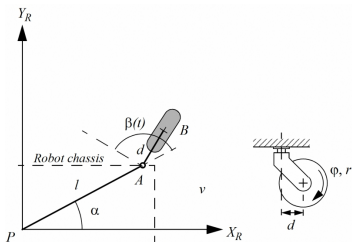
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- ▶ The sliding and rolling constraint are the same for a steered standard wheel (with a variable β)



Caster Wheel Constraints



Caster Wheel Constraints

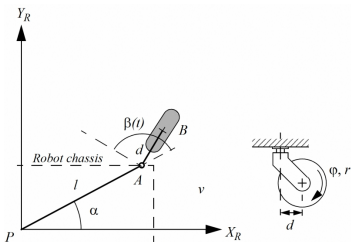


- ▶ A caster wheel differs from a steered standard wheel in its vertical rotation axis, which **does not coincide with the wheel's contact point with the ground**

- ▶ This offset has no effect on the rolling constraint on the wheel:

Rolling constraint for a caster wheel

$$\begin{pmatrix} \sin(\alpha + \beta) & -\cos(\alpha + \beta) & -l \cos(\beta) \end{pmatrix} {}^R_I R(\theta)^I \dot{\mathbf{p}} = r \dot{\varphi}$$



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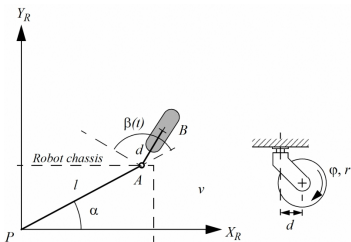
Rolling constraint for a caster wheel

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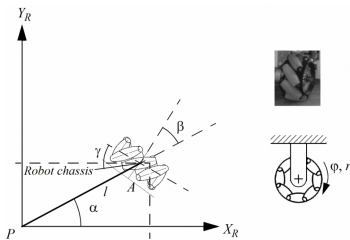
- ▶ The offset allows lateral motion, such that a steering motion can counteract any motion orthogonal to the wheel's axis (caused by a force at the caster attachment point A):

Sliding constraint for a caster wheel

$$\begin{pmatrix} \cos(\alpha + \beta) & \sin(\alpha + \beta) & d + l \sin(\beta) \end{pmatrix} {}^R R(\theta)^I \dot{\mathbf{p}} = -d \dot{\beta}$$



Swedish Wheel Constraints



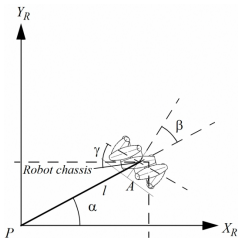
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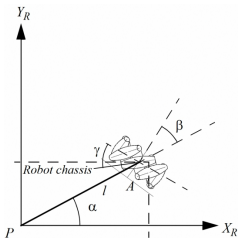
- ▶ Unlike a standard wheel, **a Swedish wheel does not have a vertical axis of rotation**
- ▶ Its rolling constraint is expressed with respect to an axis at the contact point of the rollers with the ground, which is where rolling occurs:

Rolling constraint for a Swedish wheel

$$\begin{pmatrix} \sin(\alpha + \beta + \gamma) & -\cos(\alpha + \beta + \gamma) & -l \cos(\beta + \gamma) \end{pmatrix} {}^R_I R(\theta)^T \dot{\mathbf{p}} = r \dot{\varphi} \cos(\gamma)$$



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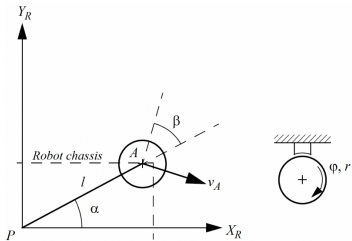
$$(\sin(\alpha + \beta + \gamma) \quad -\cos(\alpha + \beta + \gamma) \quad -l \cos(\beta + \gamma)) {}^R_I R(\theta)^I \dot{\mathbf{p}} = r \dot{\varphi} \cos(\gamma)$$

- ▶ As rollers can rotate freely with a velocity $\dot{\varphi}_{sw}$, the orthogonal motion with respect to the roller axis is not constrained; this is expressed as

Sliding constraint for a Swedish wheel

$$(\cos(\alpha + \beta + \gamma) \quad \sin(\alpha + \beta + \gamma) \quad l \sin(\beta + \gamma)) {}^R_I R(\theta)^I \dot{\mathbf{p}} = r \dot{\varphi} \sin(\gamma) + r_{sw} \dot{\varphi}_{sw}$$

Spherical Wheel Constraints



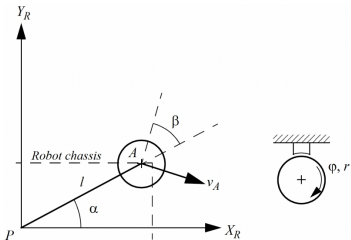
Spherical Wheel Constraints



- ▶ A spherical wheel has no concrete axis of rotation, so its constraints are defined based on conventions
- ▶ The rolling constraint expresses the rolling in the wheel's direction of motion:

Rolling constraint for a spherical wheel

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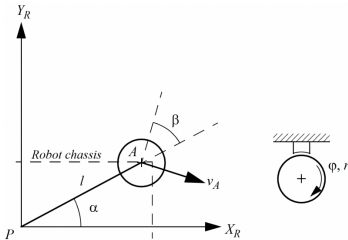
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- ▶ The sliding constraint expresses that the wheel does not move orthogonally to the direction of motion:

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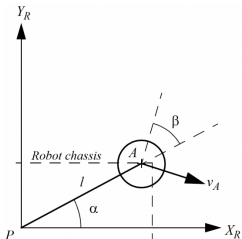
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- ▶ NB: Mathematically, these are the same as for a standard wheel, but they are interpreted differently because **a spherical wheel does not pose any constraints on a robot's motion**



- ▶ To express the kinematic constraints of a mobile robot base, **only fixed and steered standard wheels need to be taken into account** — caster, Swedish, and spherical wheels put no constraints on the motion
- ▶ Let us consider **a mobile robot base with $N = N_f + N_s$ standard wheels**, with N_f the number of fixed standard wheels and N_s the number of steered standard wheels
 - ▶ We combine the motion of these into a common vector $\dot{\varphi} = (\dot{\varphi}_f \ \dot{\varphi}_s)^T$
- ▶ The rolling and sliding constraints for the base are expressed by combining the constraints of the standard wheels

- ▶ The sliding constraint is also **a system combining the sliding constraints of the N standard wheels**; this is expressed as follows:

$$C(\beta_s)_I^R R(\theta)^I \mathbf{p} = \mathbf{0}$$

where

$$C(\beta_s) = \begin{pmatrix} C_f \\ C_s(\beta_s) \end{pmatrix}$$

Instantaneous Center of Rotation (ICR)



- ▶ The point around which a mobile robot base rotates is determined by the constraints imposed by its wheels
- ▶ This point is the **instantaneous center of rotation (ICR)** that we already encountered for a differential drive robot
- ▶ The ICR can be determined by drawing motion lines perpendicularly through the wheel axes; **the intersection point of these lines is the ICR**
 - ▶ If the wheels move in a straight line, the ICR is at infinity
- ▶ It should be noted that **not all standard wheels provide independent constraints for determining the ICR**
 - ▶ For a car, the back wheels are fixed along the same axis, so they do not both independently constrain the vehicle's motion

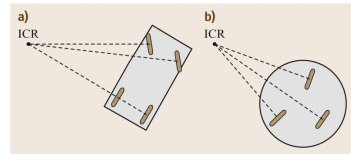


Fig.24.5a,b The instantaneous center of rotation. (a) A car-like robot; (b) a three-steering-wheels robot

Degree of Mobility

- ▶ **The number of independent sliding constraints on a mobile base is determined by the rank of $C(\beta_s)$, which we denote by $\text{rank}(C(\beta_s))$**
 - ▶ As a wheeled robot moves on a plane, we have that $0 \leq \text{rank}(C(\beta_s)) \leq 3$



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- ▶ The **degree of mobility** δ_m of a mobile robot is defined in terms of the null space of $C(\beta_s)$, which is a function of $\text{rank}(C(\beta_s))$:

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 - ▶ A bicycle has $\delta_m = 1$: at any point, it can either move forward or change its rotation

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 - ▶ A bicycle has $\delta_m = 1$: at any point, it can either move forward or change its rotation
 - ▶ A differential drive has $\delta_m = 2$: both the linear speed and orientation can be controlled instantaneously

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 - ▶ A bicycle has $\delta_m = 1$: at any point, it can either move forward or change its rotation
 - ▶ A differential drive has $\delta_m = 2$: both the linear speed and orientation can be controlled instantaneously
 - ▶ A robot without standard wheels has $\delta_m = 3$

Degree of Mobility



- ▶ The number of independent sliding constraints on a mobile base is determined by the rank of $C(\beta_s)$, which we denote by $\text{rank}(C(\beta_s))$
 - ▶ As a wheeled robot moves on a plane, we have that $0 \leq \text{rank}(C(\beta_s)) \leq 3$
- ▶ The **degree of mobility** δ_m of a mobile robot is defined in terms of the null space of $C(\beta_s)$, which is a function of $\text{rank}(C(\beta_s))$:

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- ▶ The degree of mobility determines the **differentiable degrees of freedom** (DDOF), which is the number of velocities that can be independently achieved by a robot

Degree of Steerability



- ▶ The **degree of steerability** δ_s of a mobile robot is defined as the number of steerable parameters that can be independently controlled



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- ▶ δ_s is typically defined so that $0 \leq \delta_s \leq 2$; if there are more than two steered wheels, the existence of an ICR may not be guaranteed!

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 - ▶ the degrees of freedom whose control is made possible through steering
- ▶ δ_M is thus defined as a combination of the degrees of mobility and steerability:

$$\delta_M = \delta_m + \delta_s$$

Basic Types of Wheeled Mobile Robots



Type	Maneuverability	Description
(3,0)	$\delta_M = 3, \delta_m = 3, \delta_s = 0$	No fixed or steering wheels

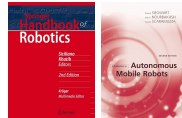


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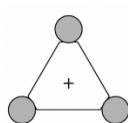


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(1,2)	$\delta_M = 3, \delta_m = 1, \delta_s = 2$	Two or more steering wheels; no fixed wheels

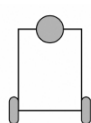
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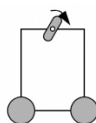
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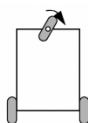
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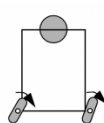
Differential
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Omni-Steer
 $\delta_M = 3$
 $\delta_m = 2$
 $\delta_s = 1$



Tricycle
 $\delta_M = 2$
 $\delta_m = 1$
 $\delta_s = 1$



Two-Steer
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- ▶ Nonholonomic constraints are nonintegrable and thus express a dependence on the body's state on the path taken to reach that state
- ▶ The sliding constraint of standard wheels is a nonholonomic constraint

Workspace, Paths, Trajectories



When considering robots in terms of their control, it is important to consider what states they can (and cannot) achieve, and how



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The workspace is the **set of all achievable configurations (poses) by a mobile robot**

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A trajectory combines a path with time, namely it is **a collection of poses along with time instants at which those poses should be reached**



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- ▶ Furthermore, various nonholonomic platforms (with $\delta_M < 3$) are able to achieve $DOF = 3$, so they are still practically useful
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 - ▶ For instance, a car has $\delta_M = 2$, but it is a very useful mobile base (obviously)
- ▶ Practically speaking, **mobile bases with varying maneuverabilities differ in the manner in which they are controlled**: a base with lower maneuverability typically requires multiple maneuvers to follow certain paths and may not be able to follow arbitrary trajectories